


Books

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- W. C. Carrara, R. G. Goodman, R. M. Majewski, Spotlight Synthetic Aperture Radar: Signal Processing Algorithms, Artech House, Boston, 1995.
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- I.G. Cumming and F.H. Wong, Digital Processing of SAR Data: Algorithms and Implementation, Artech House, 2005

Outline

1. introduction, history, frequency bands, dB, real-aperture imaging
2. radar systems: stepped-frequency systems, I/Q demodulation
3. 1D scattering by perfect conductor
4. receiver design, matched filtering
5. ambiguity function & its properties
6. range-doppler (unfocused) imaging
-  7. introduction to 3D scattering
8. ISAR
9. antenna theory
10. spotlight SAR
11. stripmap SAR
12. time permitting: deramp processing, Doppler from successive pulses

3D Mathematical Model

- We *should* use Maxwell's equations;
but instead we use

$$\left(\nabla^2 - \frac{1}{c^2(\mathbf{x})} \partial_t^2 \right) \mathcal{E}(t, \mathbf{x}) = \underbrace{j(t, \mathbf{x})}_{\text{source}}$$

- Scattering is due to a perturbation in the wave speed c :

$$\frac{1}{c^2(\mathbf{x})} = \frac{1}{c_0^2} - \underbrace{V(\mathbf{x})}_{\text{reflectivity function}}$$

- For a moving target, use $V(\mathbf{x}, t)$.

Basic facts about the wave equation

- fundamental solution g

$$(\nabla^2 - c_0^{-2} \partial_t^2) g(t, \mathbf{x}) = -\delta(t) \delta(\mathbf{x})$$

$$g(t, \mathbf{x}) = \frac{\delta(t - |\mathbf{x}|/c_0)}{4\pi|\mathbf{x}|} = \int \frac{e^{-i\omega(t-|\mathbf{x}|/c_0)}}{8\pi^2|\mathbf{x}|} d\omega$$

- $g(t, \mathbf{x})$ = field at (t, \mathbf{x}) due to a source at the origin at time 0
- Solution of

$$(\nabla^2 - c_0^{-2} \partial_t^2) u(t, \mathbf{x}) = j(t, \mathbf{x}),$$

is

$$u(t, \mathbf{x}) = - \int g(t - t', \mathbf{x} - \mathbf{y}) j(t', \mathbf{y}) dt' d\mathbf{y}$$

- frequency domain: $k = \omega/c_0$

$$(\nabla^2 + k^2)G = -\delta \quad G(\omega, \mathbf{x}) = \frac{e^{ik|\mathbf{x}|}}{4\pi|\mathbf{x}|}$$

Introduction to scattering theory

$$\begin{aligned}(\nabla^2 - c^{-2}(\mathbf{x})\partial_t^2) \mathcal{E}(t, \mathbf{x}) &= j(t, \mathbf{x}) \\ (\nabla^2 - c_0^{-2}\partial_t^2) \mathcal{E}^{in}(t, \mathbf{x}) &= j(t, \mathbf{x})\end{aligned}$$

write $\mathcal{E} = \mathcal{E}^{in} + \mathcal{E}^{sc}$, $c^{-2}(\mathbf{x}) = c_0^{-2} - V(\mathbf{x})$, subtract:

$$(\nabla^2 - \partial_t^2) \mathcal{E}^{sc}(t, \mathbf{x}) = -V(\mathbf{x})\partial_t^2 \mathcal{E}(t, \mathbf{x})$$

use fundamental solution \Rightarrow

$$\mathcal{E}^{sc}(t, \mathbf{x}) = \int g(t - \tau, \mathbf{x} - \mathbf{z}) V(\mathbf{z}) \partial_\tau^2 \mathcal{E}(\tau, \mathbf{z}) d\tau d\mathbf{z}.$$

Lippman-Schwinger integral equation

frequency domain Lippman-Schwinger equation:

$$E^{sc}(\omega, \mathbf{x}) = - \int G(\omega, \mathbf{x} - \mathbf{z}) V(\mathbf{z}) \omega^2 E(\omega, \mathbf{z}) d\mathbf{z}$$

single-scattering or *Born* approximation

$$\mathcal{E}^{sc}(t, \mathbf{x}) \approx \mathcal{E}_B^{sc} := \int g(t - \tau, \mathbf{x} - \mathbf{z}) V(\mathbf{z}) \partial_\tau^2 \mathcal{E}^{in}(\tau, \mathbf{z}) d\tau d\mathbf{z}$$

useful: makes inverse problem linear

not necessarily a good approximation!

In the frequency domain,

$$E_B^{sc}(\omega, \mathbf{x}) = - \int \frac{e^{ik|\mathbf{x}-\mathbf{z}|}}{4\pi|\mathbf{x}-\mathbf{z}|} V(\mathbf{z}) \omega^2 E^{in}(\omega, \mathbf{z}) d\mathbf{z}$$

E^{in} is obtained by solving $(\nabla^2 + k^2)E^{in} = J$

For now, suppose $J(\omega, \mathbf{x}) = P(\omega)\delta(\mathbf{x} - \mathbf{x}^0) \Rightarrow$

$$E^{in}(\omega, \mathbf{x}) = - \int G(\omega, \mathbf{x} - \mathbf{y}) P(\omega) \delta(\mathbf{y} - \mathbf{x}^0) dt' d\mathbf{y} = -P(\omega) \frac{e^{ik|\mathbf{x} - \mathbf{x}^0|}}{4\pi|\mathbf{x} - \mathbf{x}^0|}$$

Then the scattered field back at \mathbf{x}_0 is

$$E_B^{sc}(\omega, \mathbf{x}^0) = P(\omega) \omega^2 \int \frac{e^{2ik|\mathbf{x}^0 - \mathbf{z}|}}{(4\pi)^2 |\mathbf{x}^0 - \mathbf{z}|^2} V(\mathbf{z}) d\mathbf{z}$$

In the time domain this is

$$\mathcal{E}_B^{sc}(t, \mathbf{x}^0) = \int \frac{e^{-i\omega(t-2|\mathbf{x}^0 - \mathbf{z}|/c)}}{2\pi(4\pi|\mathbf{x}^0 - \mathbf{z}|)^2} k^2 P(\omega) V(\mathbf{z}) d\omega d\mathbf{z}$$

Note $1/R^2$ geometrical decay \Rightarrow power decays like $1/R^4$

Matched filtering

$$\begin{aligned}
 \eta(t, \mathbf{x}^0) &\approx \int p^*(t' - t) \mathcal{E}_B^{sc}(t', \mathbf{x}^0) dt' \\
 &= \int \left(\frac{1}{2\pi} \int e^{i\omega'(t' - t)} P(\omega') d\omega' \right) \\
 &\quad \cdot \int \frac{e^{-i\omega(t' - 2|\mathbf{x}^0 - \mathbf{z}|/c)}}{2\pi(4\pi|\mathbf{x}^0 - \mathbf{z}|)^2} k^2 P(\omega) V(\mathbf{z}) d\omega d\mathbf{z} dt' \\
 &\quad \vdots \quad \text{do } t' \text{ and } \omega' \text{ integrations} \\
 &= \int \frac{e^{-i\omega(t - 2|\mathbf{x}^0 - \mathbf{z}|/c)}}{2\pi(4\pi|\mathbf{x}^0 - \mathbf{z}|)^2} k^2 |P(\omega)|^2 V(\mathbf{z}) d\omega d\mathbf{z}
 \end{aligned}$$

Effect of matched filter is to replace $P(\omega)$ by $|P(\omega)|^2$.

Far-field expansion

$$|z| \ll |x^0| \quad \Rightarrow \quad |x^0 - z| = |x^0| - \widehat{x^0} \cdot z + O(|x^0|^{-1})$$

where $\widehat{x} = x/|x|$

Proof:

$$\begin{aligned} |x^0 - z| &= \sqrt{(x^0 - z) \cdot (x^0 - z)} = \sqrt{|x^0|^2 - 2x^0 \cdot z + |z|^2} \\ &= |x^0| \sqrt{1 - 2 \frac{x^0 \cdot z}{|x^0|^2} + \frac{|z|^2}{|x^0|^2}} \quad \text{use } \sqrt{1 - a} = 1 - \frac{a}{2} + \dots \\ &= |x^0| \left(1 - \frac{\widehat{x^0} \cdot z}{|x^0|} + O(|x^0|^{-2}) \right) \\ &= |x^0| - \widehat{x^0} \cdot z + O\left(\frac{|z|}{|x^0|}\right) \end{aligned}$$

Note: Whether $|z| \ll |x^0|$ depends on location of origin of coordinates.

$$\frac{e^{ik|x^0 - z|}}{|x^0 - z|} = \frac{e^{ik|x^0|}}{|x^0|} e^{-ik\widehat{x^0} \cdot z} \left(1 + O\left(\frac{|z|}{|x^0|}\right) \right) \left(1 + O\left(\frac{k|z|^2}{|x^0|}\right) \right)$$

Far-field approximation to data

applies to smallish target

(Born-approximated) output of correlation receiver is:

$$\eta_B(t, \mathbf{x}^0) = \int \frac{e^{-i\omega(t-2|\mathbf{x}^0-\mathbf{z}|/c)}}{2\pi(4\pi|\mathbf{x}^0-\mathbf{z}|)^2} k^2 |P(\omega)|^2 V(\mathbf{z}) d\omega d\mathbf{z}$$


put origin of coordinates in target, use far-field expansion \Rightarrow

$$\eta_B(t, \mathbf{x}^0) \approx \frac{1}{32\pi^2|\mathbf{x}^0|^2} \int e^{-i\omega(t-2|\mathbf{x}^0|/c+2\widehat{\mathbf{x}}^0 \cdot \mathbf{z}/c)} k^2 |P(\omega)|^2 V(\mathbf{z}) d\omega d\mathbf{z}$$

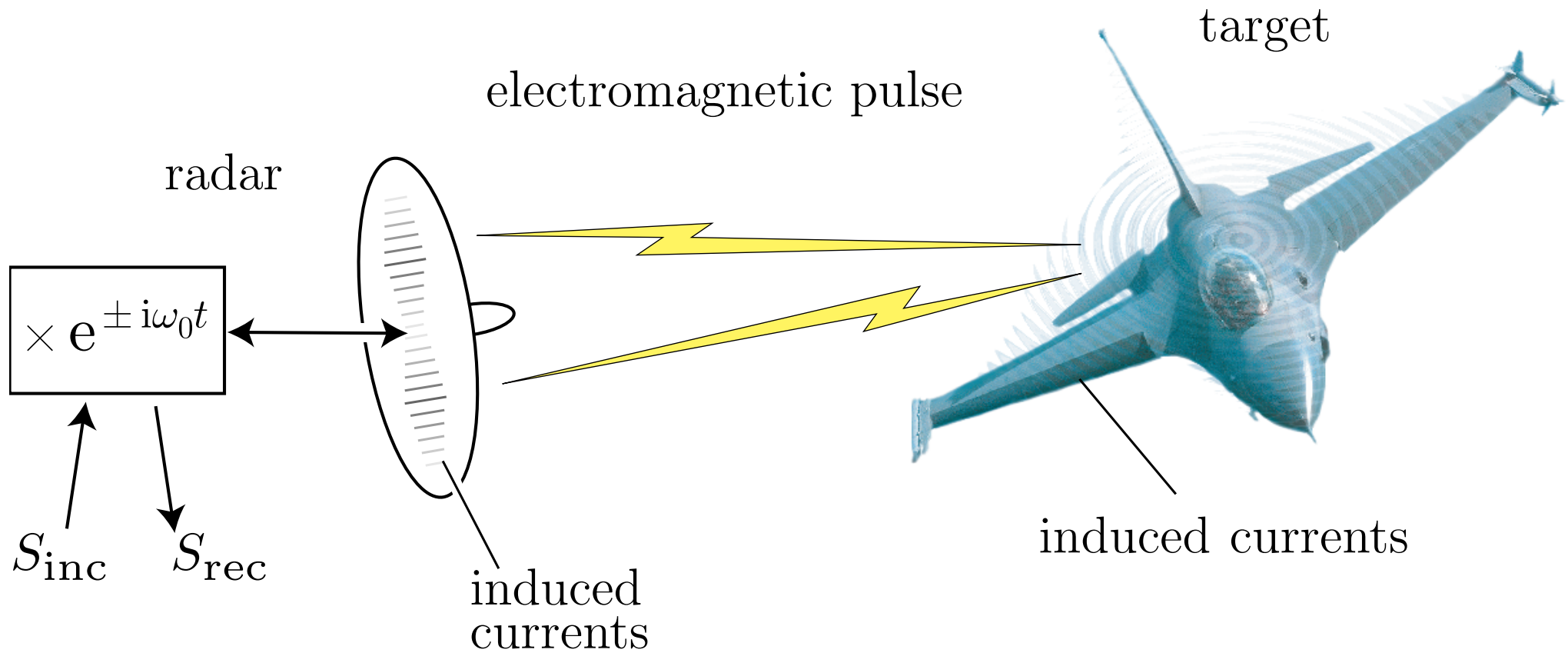
in the frequency domain:

$$D_B(\omega, \mathbf{x}^0) \approx \frac{e^{2ik|\mathbf{x}^0|}}{32\pi^2|\mathbf{x}^0|^2} k^2 |P(\omega)|^2 \underbrace{\int e^{2ik\widehat{\mathbf{x}}^0 \cdot \mathbf{z}} V(\mathbf{z}) d\mathbf{z}}_{\mathcal{F}[V](2k\widehat{\mathbf{x}}^0) !}$$

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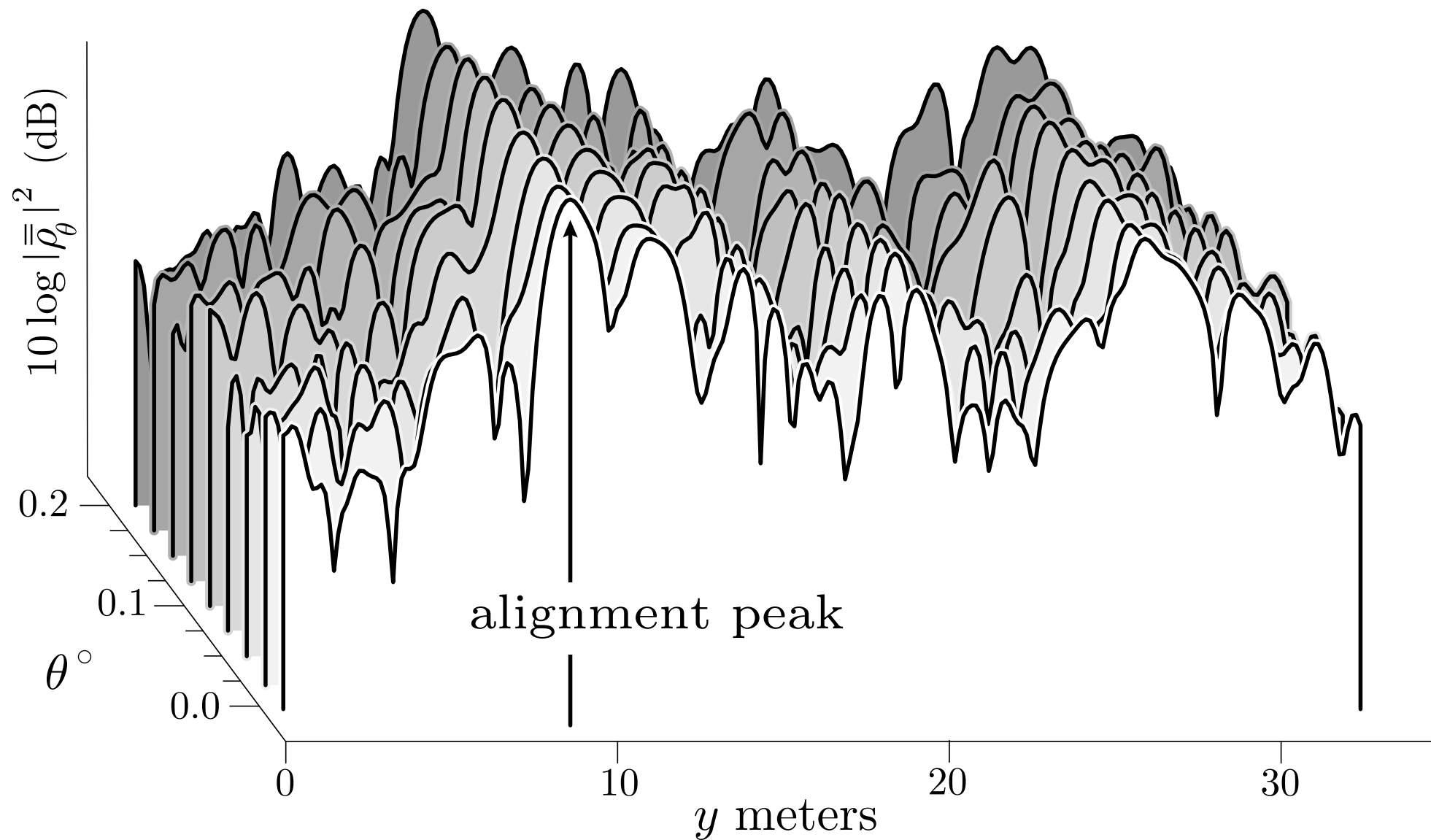
Airborne targets



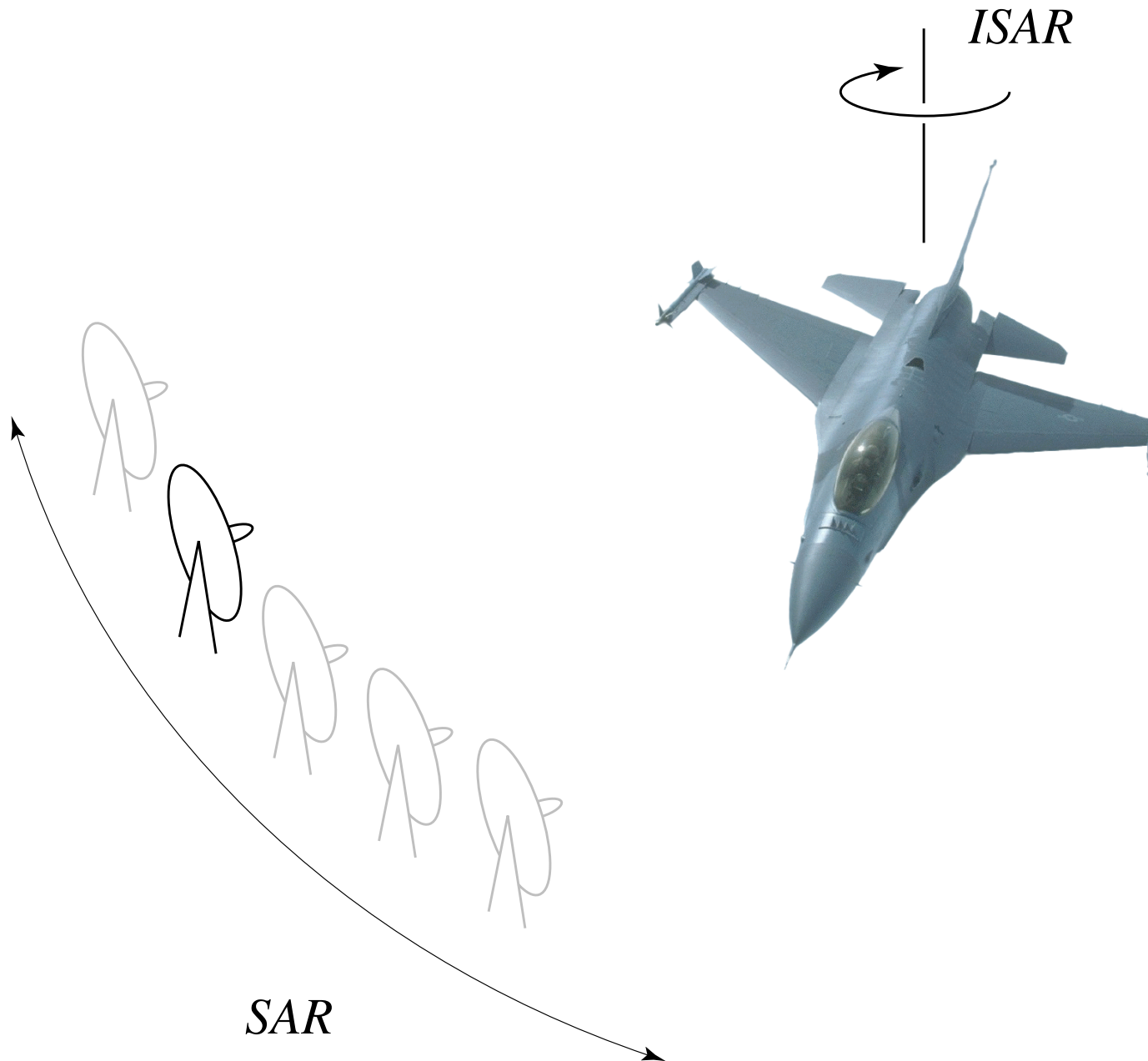
Inverse Synthetic Aperture Radar (ISAR)

- fixed radar, moving target (usually airplane or ship)
- transmit pulse train
- typical pulse length $\approx 10^{-4}$ sec,
rotation rate $\Omega = 10^\circ/\text{sec} \approx 1/6 \text{ R/sec}$, target radius $\approx 10\text{m} \Rightarrow$
distance traveled during pulse $\approx 10^{-4}m \Rightarrow$ start-stop approximation
- for airborne target, measurements from n th pulse contain no reflections from earlier pulses
- take out translational motion via tracking and *range alignment*, leaving only rotational motion

Range alignment



ISAR vs SAR



Mathematics of ISAR

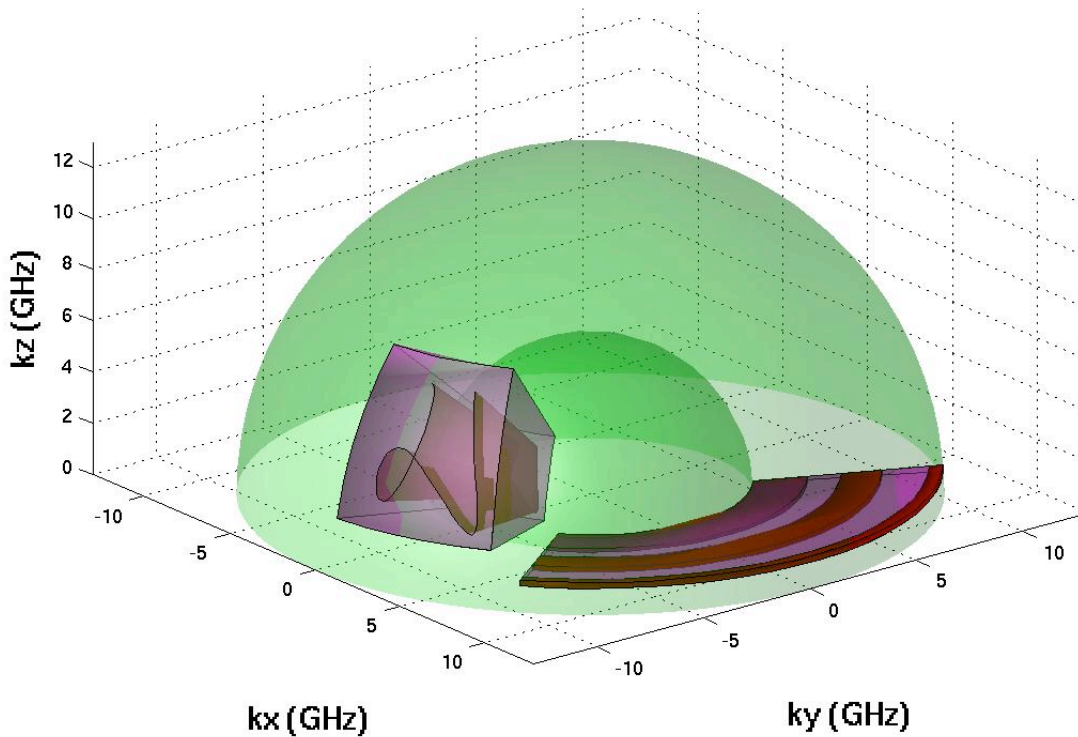
at start of n th pulse, $V(\mathbf{x}) = q(\mathcal{O}(\theta_n)\mathbf{x})$ where \mathcal{O} is an orthogonal matrix

For example: if radar is in plane \perp to axis of rotation (“turntable geometry”),

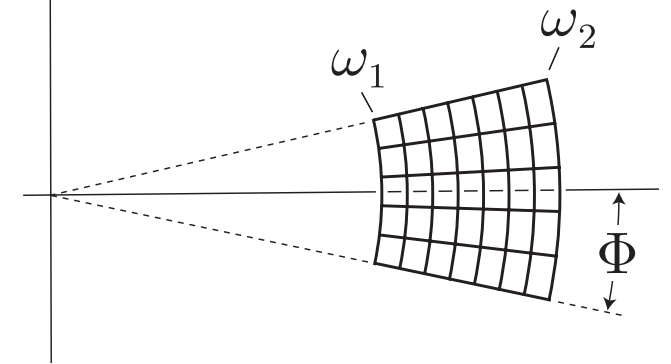
$$\mathcal{O}(\theta) = \begin{pmatrix} \cos \theta & -\sin \theta & 0 \\ \sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$\begin{aligned} D_B(\omega, \theta_n) &\approx \frac{e^{2ik|\mathbf{x}^0|}}{32\pi^2|\mathbf{x}^0|^2} k^2 |P(\omega)|^2 \int e^{2ik\widehat{\mathbf{x}}^0 \cdot \mathbf{z}} \underbrace{q(\mathcal{O}(\theta_n)\mathbf{z})}_{\mathbf{y}} d\mathbf{z} \\ &\quad (\text{ use } \mathbf{x}^0 \cdot \mathcal{O}^{-1}(\theta_n)\mathbf{y} = \mathcal{O}(\theta_n)\mathbf{x}^0 \cdot \mathbf{y}) \\ &= \frac{e^{2ik|\mathbf{x}^0|}}{32\pi^2|\mathbf{x}^0|^2} k^2 |P(\omega)|^2 \underbrace{\int e^{2ik\mathcal{O}(\theta_n)\widehat{\mathbf{x}}^0 \cdot \mathbf{y}} V(\mathbf{y}) d\mathbf{y}}_{\mathcal{F}[q](2k\mathcal{O}(\theta_n)\widehat{\mathbf{x}}^0) !} \end{aligned}$$

Region in Fourier space where we have data



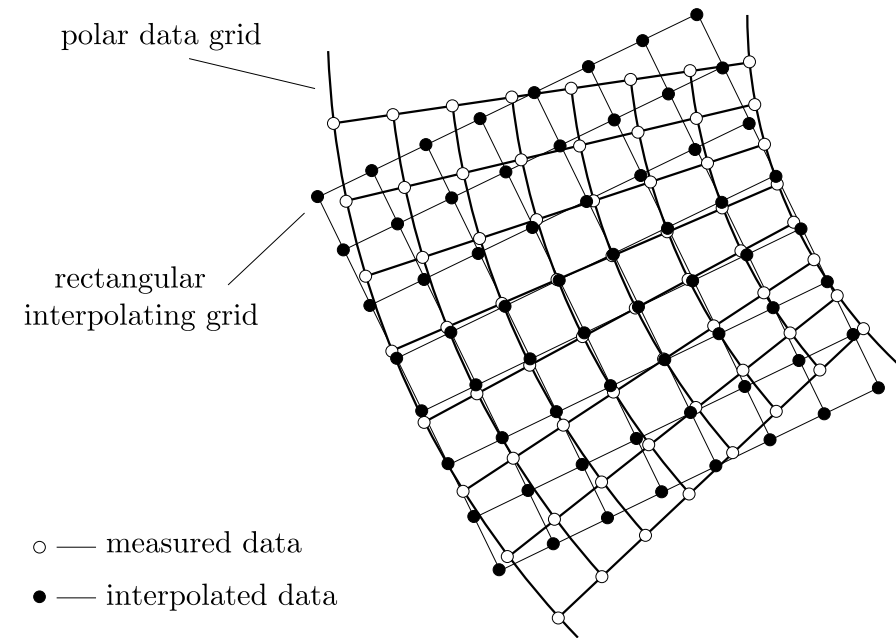
The backhoe data dome



Ω (turntable geometry)

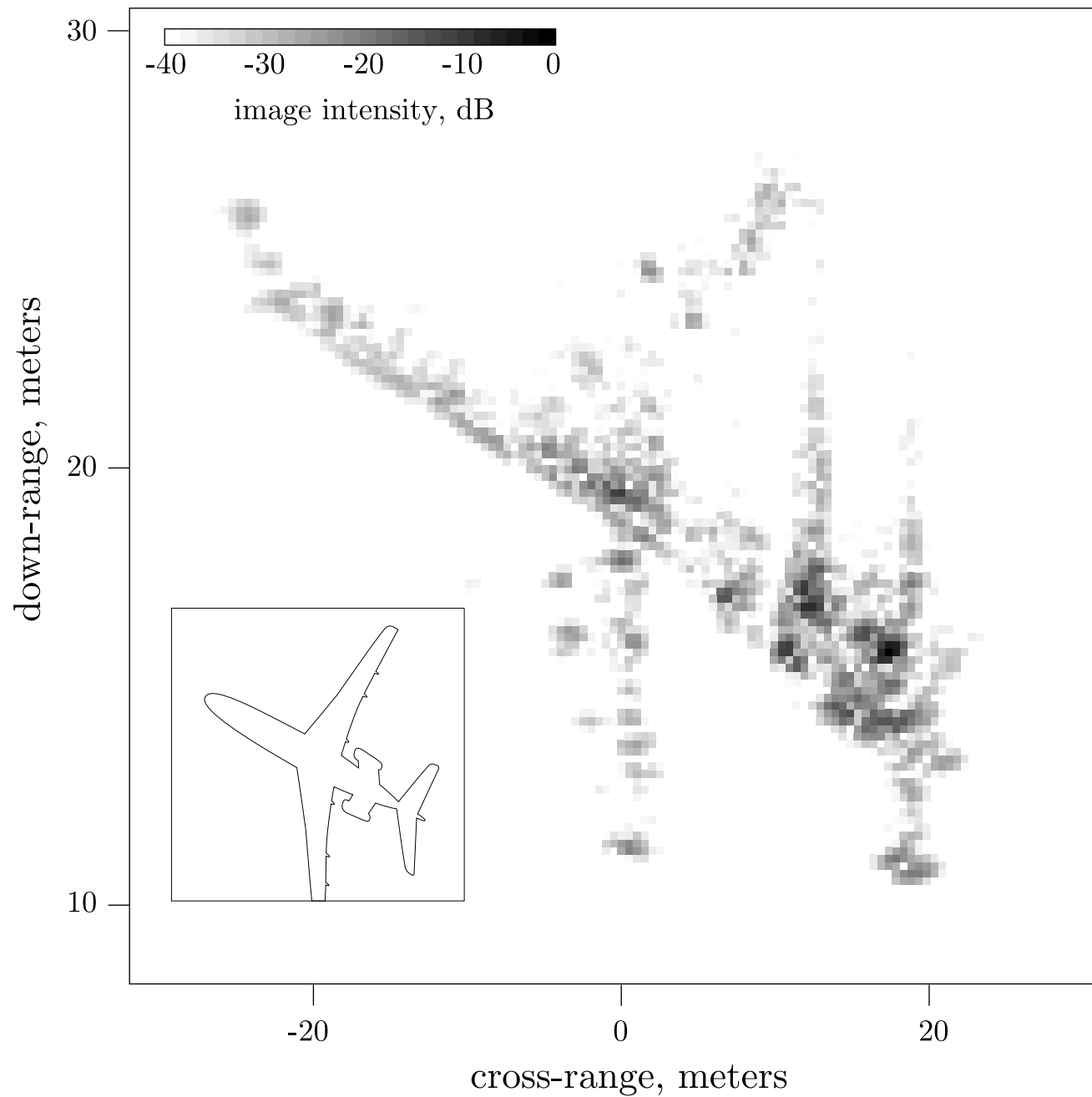
Polar Format Algorithm (PFA)

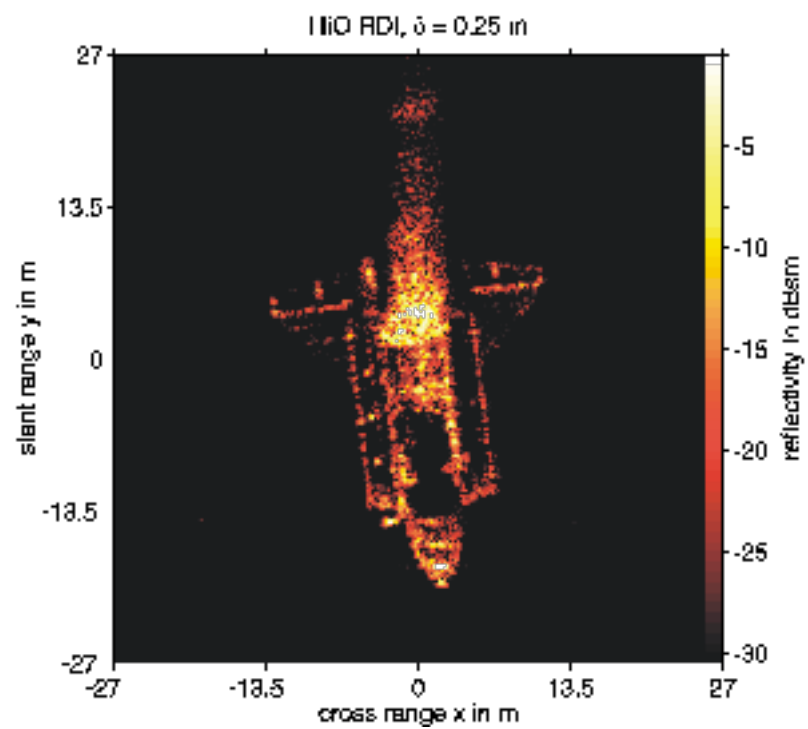
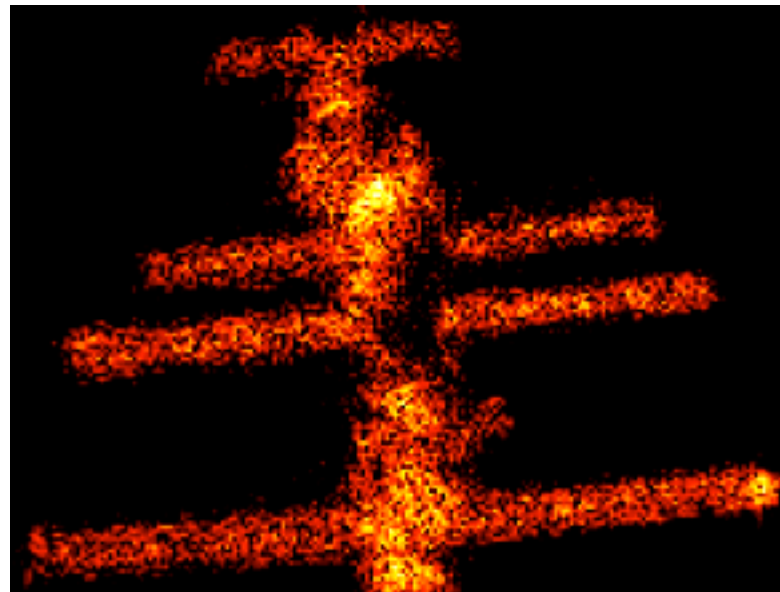
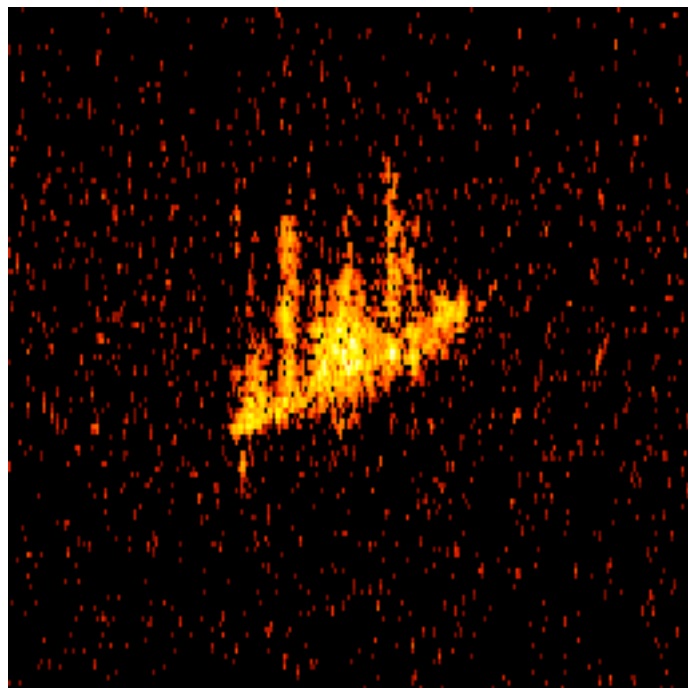
applies to turntable geometry, frequency-domain data



1. interpolate to rectangular grid
2. use 2D Fast Fourier Transform

An ISAR image of a Boeing 727 taking off from LAX

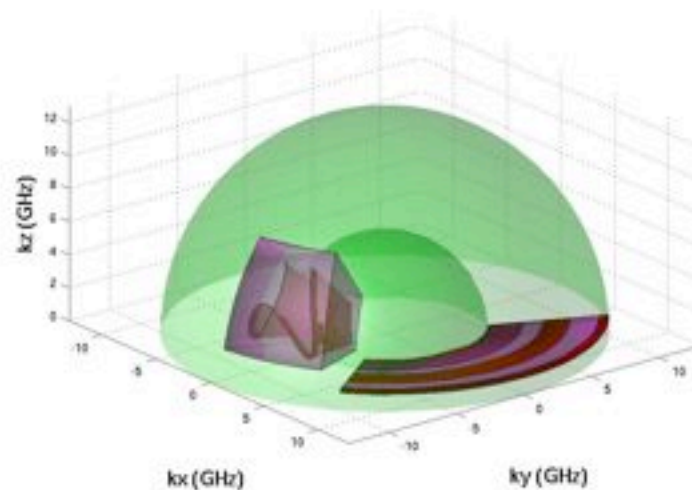


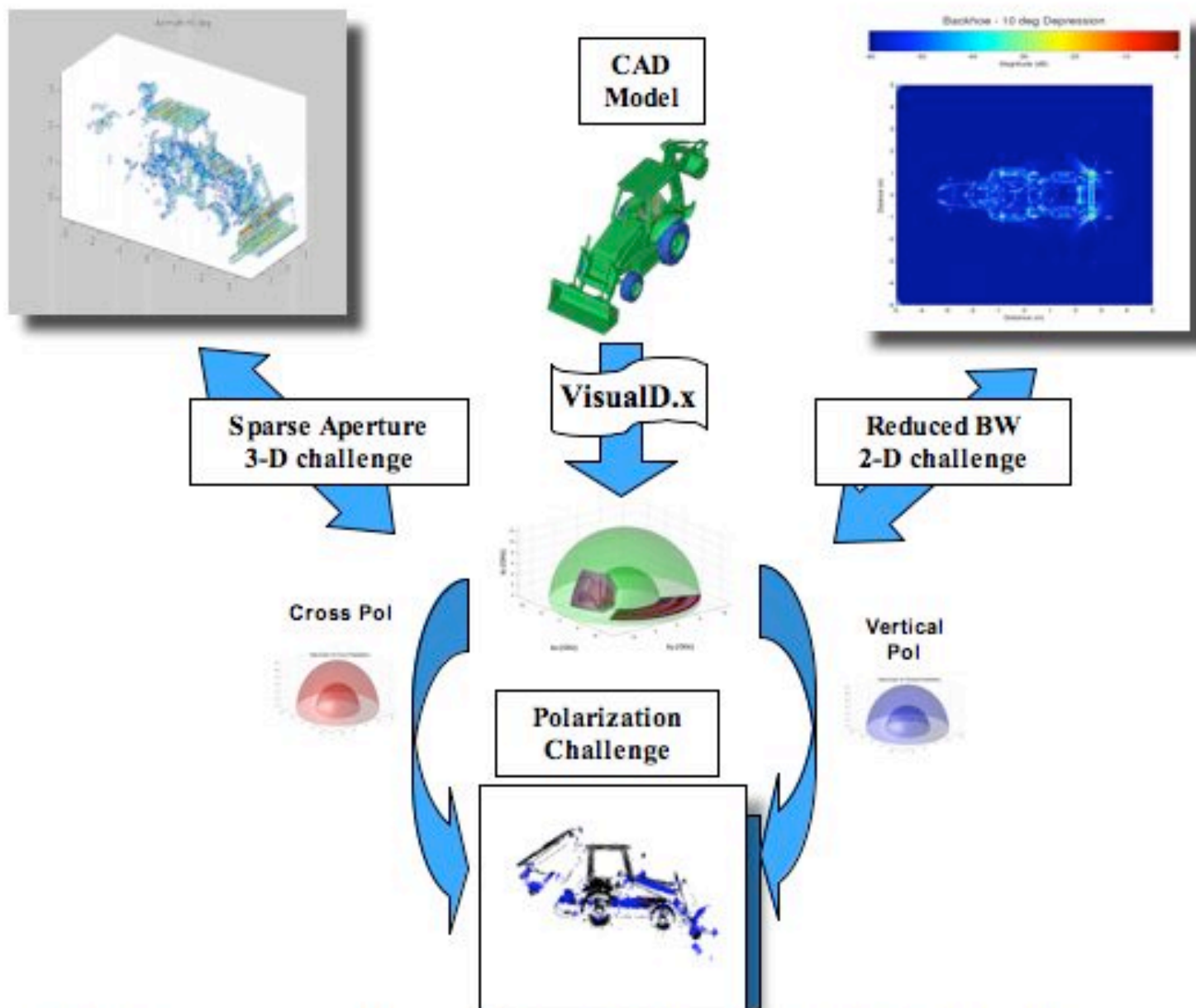


Mir



Backhoe Sample Public Release VISUAL-D Challenge Problem





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ISAR Resolution – Notation

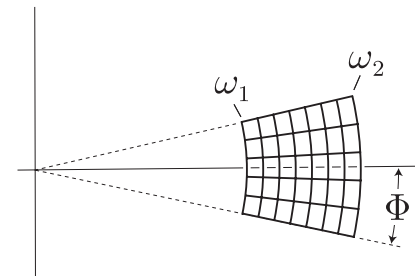
Assume turntable geometry

Take $\mathbf{x}^0 = (1, 0, 0)$, write $\hat{\mathbf{e}}_\theta = \mathcal{O}(\theta)\mathbf{x}^0$.

$$\begin{aligned}\tilde{D}(k, \theta) &= \int e^{-2ik(y_1 \cos \theta + y_2 \sin \theta)} q(y_1, y_2, y_3) dy_1 dy_2 dy_3 \\ &\quad \int e^{-2ik(y_1 \cos \theta + y_2 \sin \theta)} \underbrace{\int q(y_1, y_2, y_3) dy_3}_{\tilde{q}(y_1, y_2)} dy_1 dy_2\end{aligned}$$

get 2D image of \tilde{q} = target projected onto plane containing radar

ISAR Resolution, continued



$$\tilde{D}(k, \theta) = \chi_{\Omega}(k\hat{\mathbf{e}}_{\theta})\mathcal{F}[q](k\hat{\mathbf{e}}_{\theta})$$

to form image, take 2D inverse Fourier transform

$$\begin{aligned} I(\mathbf{x}) &= \int e^{i\mathbf{x}\cdot k\hat{\mathbf{e}}_{\theta}} \tilde{D}(k, \theta) k dk d\theta = \int e^{i\mathbf{x}\cdot k\hat{\mathbf{e}}_{\theta}} \int_{\Omega} e^{-i\mathbf{y}\cdot k\hat{\mathbf{e}}_{\theta}} \tilde{q}(\mathbf{y}) d\mathbf{y} k dk d\theta \\ &= \int \underbrace{\int_{\Omega} e^{i(\mathbf{x}-\mathbf{y})\cdot k\hat{\mathbf{e}}_{\theta}} k dk d\theta}_{K(\mathbf{x}-\mathbf{y})} \tilde{q}(\mathbf{y}) d^2\mathbf{y} \end{aligned}$$



point spread function (PSF), imaging kernel, ambiguity function

ISAR Resolution: analysis of PSF

$$K(\mathbf{z}) = \int_{\Omega} e^{i\mathbf{z} \cdot k \hat{\mathbf{e}}_{\theta}} k dk d\theta$$

Take $\hat{\mathbf{e}}_{\theta} = (\cos \theta, \sin \theta) \approx (1, \theta)$ (small-angle approx.)

$$\mathbf{z} = r(\cos \psi, \sin \psi) \quad b = k_2 - k_1 \quad k_c = \omega_c / c$$

Down-range resolution

$$K(r, 0) \approx \frac{2\Phi}{i} \frac{d}{dr} \left[e^{ik_c r} \frac{b}{2} \text{sinc}(br/2) \right]$$

$$K(r, 0) \approx b\omega_c \Phi e^{ik_c r} \text{sinc} \frac{br}{2}$$

down-range resolution is $4\pi/b$

note oscillatory factor

Cross-range Resolution

$$K(0, r) \approx 2bk_c\Phi \operatorname{sinc}\left(\frac{br\Phi}{2}\right) \operatorname{sinc}(k_cr\Phi)$$

$$k_c \gg b \Rightarrow$$

$$K(r, 0) \approx 2bk_c\Phi \operatorname{sinc}(k_cr\Phi)$$

cross-range resolution is $2\pi/(k_c\Phi)$

ISAR in the time domain

$$D_B(\omega, \theta_n) \approx \frac{e^{2ik|\mathbf{x}^0|}}{32\pi^2|\mathbf{x}^0|^2} k^2 |P(\omega)|^2 \underbrace{\int e^{2ik \mathcal{O}(\theta_n) \widehat{\mathbf{x}}^0 \cdot \mathbf{y}} q(\mathbf{y}) d\mathbf{y}}_{\mathcal{F}[q](2k\mathcal{O}(\theta_n) \widehat{\mathbf{x}}^0)}$$

↓ Fourier transform

$$\eta_B(t, \theta_n) \propto \int \int e^{-i\omega(t-2|\mathbf{x}^0|/c+2\mathcal{O}(\theta_n) \widehat{\mathbf{x}}^0 \cdot \mathbf{y}/c)} \omega^2 |P(\omega)|^2 d\omega q(\mathbf{y}) d\mathbf{y}$$

$$\eta_B\left(t + \frac{2|\mathbf{x}^0|}{c}, \theta_n\right) = \underbrace{\int \int e^{-i\omega(t+\overbrace{2\mathcal{O}(\theta_n) \widehat{\mathbf{x}}^0 \cdot \mathbf{y}}^{-\tau}/c)} \omega^2 |P(\omega)|^2 d\omega q(\mathbf{y}) d\mathbf{y}}_{\int \delta(s-\tau) \underbrace{\int e^{-i\omega(t-s)} \omega^2 |P(\omega)|^2 d\omega}_{\chi(t-s)} ds}$$

$$\begin{aligned}
\eta_B \left(t + \frac{2|\mathbf{x}^0|}{c}, \theta_n \right) &= \int \chi(t-s) \underbrace{\int \delta \left(s - \frac{2\mathcal{O}(\theta_n)\widehat{\mathbf{x}}^0}{c} \cdot \mathbf{y} \right) q(\mathbf{y}) d\mathbf{y}}_{\mathcal{R}[q] \left(s, \frac{2\mathcal{O}(\theta_n)\widehat{\mathbf{x}}^0}{c} \right)} ds \\
&= \chi * \mathcal{R}[q] \left(\frac{2\mathcal{O}(\theta_n)\widehat{\mathbf{x}}^0}{c} \right)
\end{aligned}$$

where $\mathcal{R}[q](s, \widehat{\boldsymbol{\mu}}) = \int \delta(s - \widehat{\boldsymbol{\mu}} \cdot \mathbf{x}) q(\mathbf{x}) d\mathbf{x}$ is the *Radon transform*

For ISAR, use waveform so that $\chi \approx \delta$ (high range-resolution waveform)

Radon transform

$$\begin{aligned}\mathcal{R}_{\hat{\boldsymbol{\mu}}}[q](s) = \mathcal{R}[q](s, \hat{\boldsymbol{\mu}}) &= \int \delta(s - \hat{\boldsymbol{\mu}} \cdot \mathbf{x}) q(\mathbf{x}) d\mathbf{x} = \int_{s=\hat{\boldsymbol{\mu}} \cdot \mathbf{x}} q(\mathbf{x}) d^n \mathbf{x} \\ &= \int_{\mathbf{x}' \perp \hat{\boldsymbol{\mu}}} q(s\hat{\boldsymbol{\mu}} + \mathbf{x}') d^{n-1} \mathbf{x}'\end{aligned}$$

Properties

- Projection-slice theorem:

$$\mathcal{F}_{s \rightarrow \sigma}(\mathcal{R}_{\hat{\boldsymbol{\mu}}}[f])(\sigma) = (2\pi)^{(n-1)/2} \mathcal{F}_n[f](\sigma \hat{\boldsymbol{\mu}})$$

↑

↑

1D Fourier transform

n D Fourier transform

here Fourier transforms have symmetric $1/\sqrt{2\pi}$ convention

- Filtered backprojection (FBP):

$$(\mathcal{R}^\# h) * f = \mathcal{R}^\# (h * \mathcal{R}[f])$$

\nearrow \uparrow
 backprojection operator filter

where $\mathcal{R}^\#$ operates on $h(s, \boldsymbol{\mu})$ via

$$(\mathcal{R}^\# h)(\boldsymbol{x}) = \int_{S^{n-1}} h(\boldsymbol{x} \cdot \hat{\boldsymbol{\mu}}, \hat{\boldsymbol{\mu}}) d\hat{\boldsymbol{\mu}}$$

- $\mathcal{R}^\#$ integrates over part of h corresponding to all lines through \boldsymbol{x}
- $\mathcal{R}^\#$ is the formal adjoint of \mathcal{R} , i.e.,

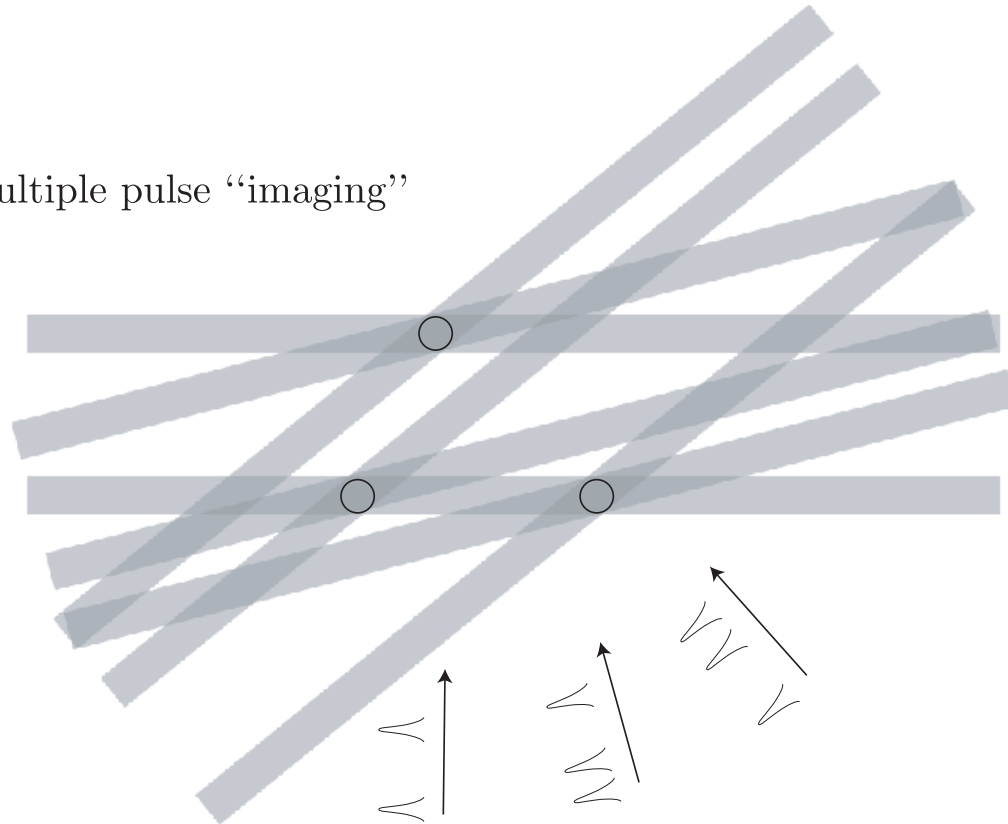
$$\langle \mathcal{R}f, h \rangle_{L^2(\mathbb{R} \times S^{n-1})} = \langle f, \mathcal{R}^\# h \rangle_{L^2(\mathbb{R}^n)}$$

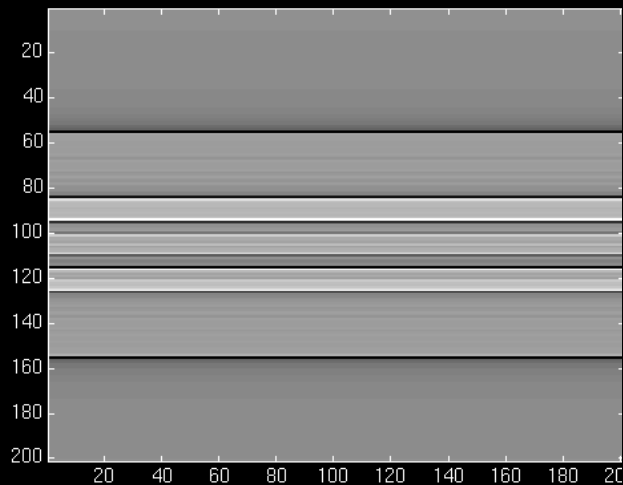
Radon transform



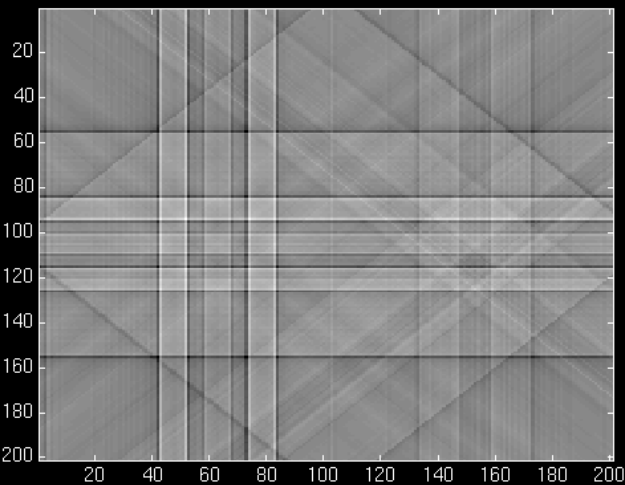
Single pulse ambiguity

Multiple pulse “imaging”

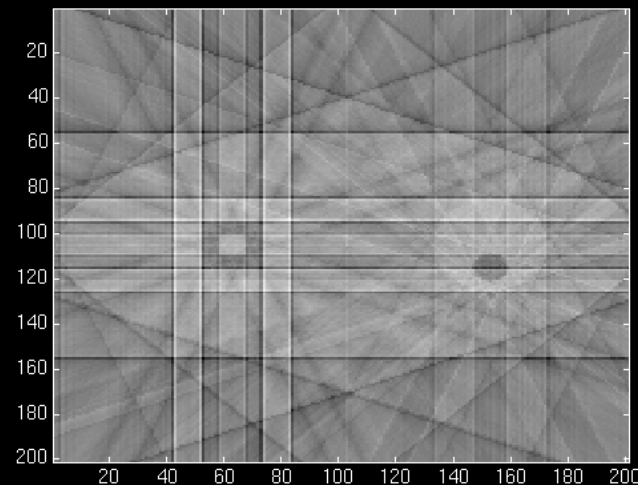




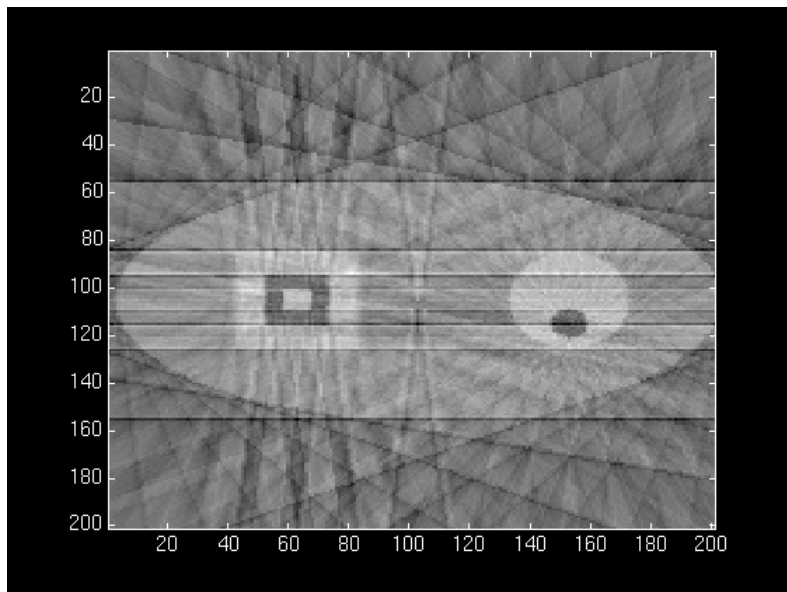
1 view



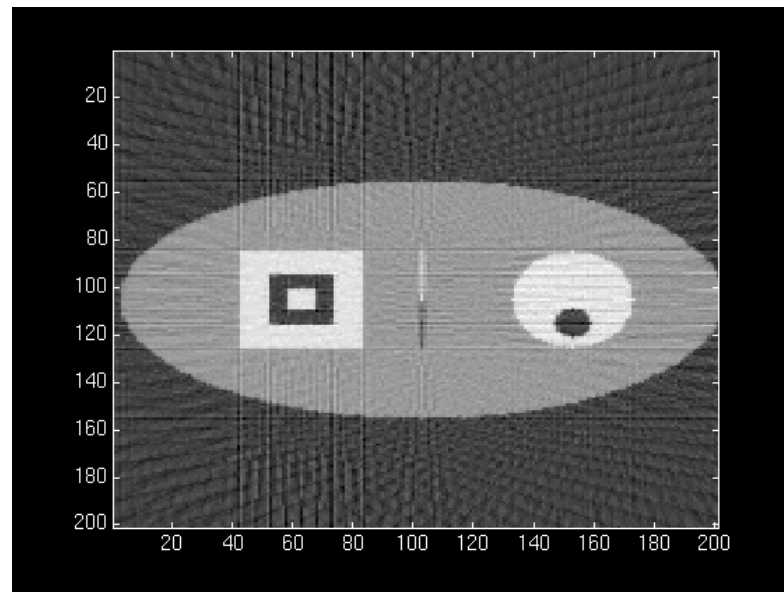
4 views



8 views



16 views



60 views

ISAR summary

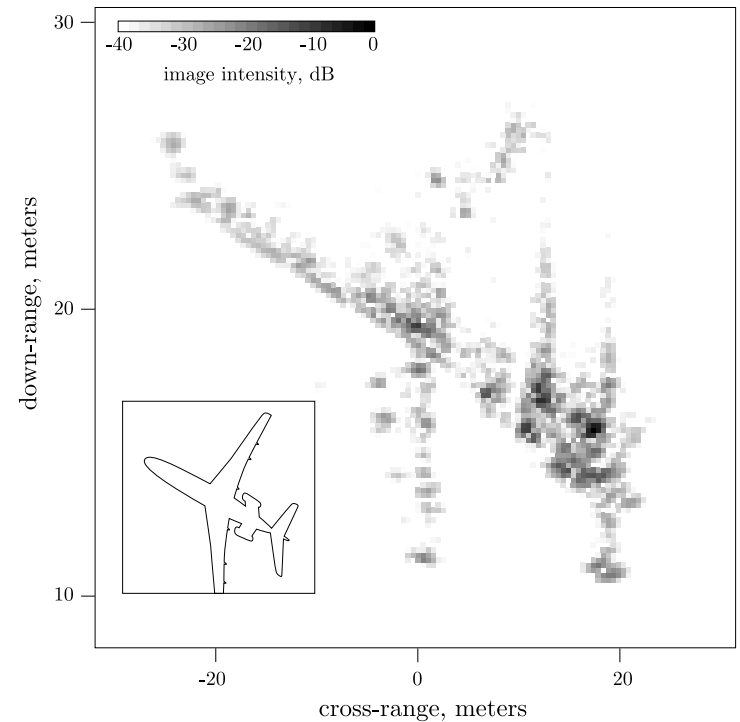
- use high range-resolution waveform (broad frequency band)
- time-domain formulation gives rise to Radon transform
 - invert via FBP or . . .
- frequency-domain formulation gives Fourier transform of target on polar grid
 - interpolate to cartesian grid, use FFT
- can make images from an aperture of a few degrees because of high carrier frequency

ISAR is sometimes called range-doppler imaging


Doppler shift can be *inferred* from phase of successive measurements

Where more work is needed on ISAR

- model; Born approximation leaves out:
 - multiple scattering
 - shadowing
 - creeping waves
- find target/sensor motion
- 3D imaging
- template library look-up
- fast algorithms



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