

We will not answer questions about this page during the exam.

f is a real-valued function and $\mathbf{F}(x, y, z) = \langle M, N, P \rangle$ is vector-valued. (If in \mathbb{R}^2 , $\mathbf{F} = \langle M, N \rangle$.)

\mathbf{T} is an appropriate unit tangent vector and \mathbf{n} is an appropriate unit normal vector.

$\mathbf{r}(t) = \langle f(t), g(t), h(t) \rangle$ is a parameterization of a curve in \mathbb{R}^3 ($\mathbf{r}(t) = \langle f(t), g(t) \rangle$ in \mathbb{R}^2);

$\mathbf{r}(u, v) = \langle f(u, v), g(u, v), h(u, v) \rangle$ is a parameterization of a surface, with $\mathbf{r}_u = \frac{\partial \mathbf{r}}{\partial u}$ and $\mathbf{r}_v = \frac{\partial \mathbf{r}}{\partial v}$.

Line Integral along a curve C : $\int_C f(x, y, z) ds = \int_a^b f(\mathbf{r}(t))|\mathbf{v}(t)| dt$, where $\mathbf{v}(t) = \mathbf{r}'(t)$.

Work/Circ/Flow along a curve C :

in \mathbb{R}^2 : Work/Circ/Flow = $\int_C \mathbf{F} \cdot d\mathbf{r} = \int_C Mdx + Ndy$. Also see Green's Theorem.

in \mathbb{R}^3 : Work/Circ/Flow = $\int_C \mathbf{F} \cdot d\mathbf{r} = \int_C Mdx + Ndy + Pdz$. Also see Stokes' Theorem.

Flux of vector field \mathbf{F} :

across curve $C \subset \mathbb{R}^2$: $\int_C \mathbf{F} \cdot \mathbf{n} ds = \int_C Mdy - Ndx$. Also see Green's Theorem.

through surface $S \subset \mathbb{R}^3$: $\iint_S \mathbf{F} \cdot \mathbf{n} d\sigma = \iint_S \mathbf{F} \cdot (\mathbf{r}_u \times \mathbf{r}_v) dudv$. Also see Divergence Theorem.

Component Test: $\frac{\partial M}{\partial y} = \frac{\partial N}{\partial x}$, $\frac{\partial M}{\partial z} = \frac{\partial P}{\partial x}$, $\frac{\partial N}{\partial z} = \frac{\partial P}{\partial y}$.

Fundamental Theorem for Line Integrals: If $\mathbf{F} = \nabla f$ and curve C goes from A to B , then

$$\int_C \mathbf{F} \cdot d\mathbf{r} = f(B) - f(A).$$

Green's Theorem: Region $R \subset \mathbb{R}^2$ has closed boundary curve C .

Work/Circ/Flow = $\oint_C \mathbf{F} \cdot d\mathbf{r} = \int_C Mdx + Ndy = \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dx dy = \iint_R \nabla \times \mathbf{F} \cdot \mathbf{k} dx dy$,

Flux = $\oint_C \mathbf{F} \cdot \mathbf{n} ds = \int_C Mdy - Ndx = \iint_R \left(\frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} \right) dx dy = \iint_R \nabla \cdot \mathbf{F} dx dy$

Surface Integral of g over the surface S ($g(x, y, z) = 1$ for surface area):

$$\iint_S g(x, y, z) d\sigma = \iint_R g(\mathbf{r}(u, v))|\mathbf{r}_u \times \mathbf{r}_v| du dv, \text{ with parameters } u, v \text{ in } R.$$

Stokes' Theorem: Surface S with closed boundary curve C .

Work/Circ/Flow = $\oint_C \mathbf{F} \cdot d\mathbf{r} = \int_C Mdx + Ndy + Pdz = \iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} d\sigma = \iint_S \nabla \times \mathbf{F} \cdot (\mathbf{r}_u \times \mathbf{r}_v) dudv$.

Divergence Theorem : Solid D with boundary surface S .

$$\text{Flux} = \iint_S \mathbf{F} \cdot \mathbf{n} d\sigma = \iint_S \mathbf{F} \cdot (\mathbf{r}_u \times \mathbf{r}_v) dudv = \iiint_D \nabla \cdot \mathbf{F} dV = \iiint_D \frac{\partial M}{\partial x} + \frac{\partial N}{\partial y} + \frac{\partial P}{\partial z} dV.$$